

ECCOMAS

Thematic Conference on Meshless Methods

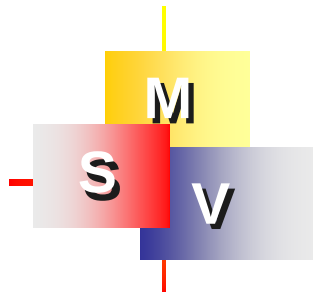
**True and spurious eigensolutions for
membrane and plate problems by using
method of fundamental solutions**

Jeng-Tzong Chen and Ying-Te Lee

Lisbon, Portugal

July 11-14, 2005

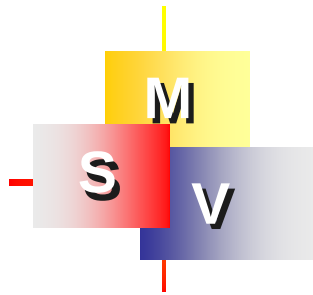
National Taiwan Ocean University, Keelung, Taiwan



Outlines

1. Introduction
2. Problem statements
3. Mathematical analysis
4. Treatment methods
5. Numerical examples
6. Conclusions

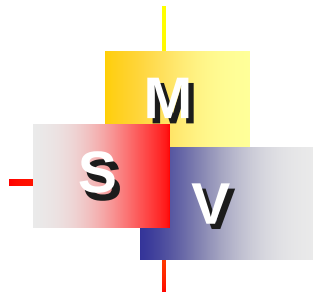




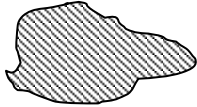
Outlines

1. Introduction
2. Problem statements
3. Mathematical analysis
4. Treatment methods
5. Numerical examples
6. Conclusions

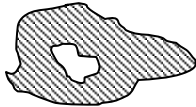




Spurious eignesolutions in BEM

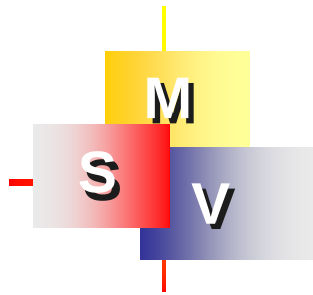
Simply-connected problem  (Membrane and plate)

	Real/MRM	Imaginary	Complex
Saving CPU time	Yes	Yes	No
Avoid singular integral	No	Yes	No
Spurious eigenvalues	Appear	Appear	No

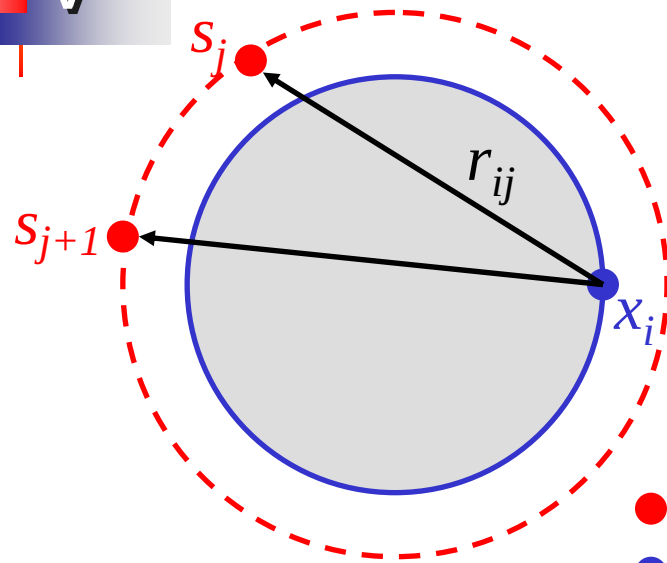
Multiply-connected problem  (Membrane and plate)

	Complex
Spurious eigenvalues	Appear

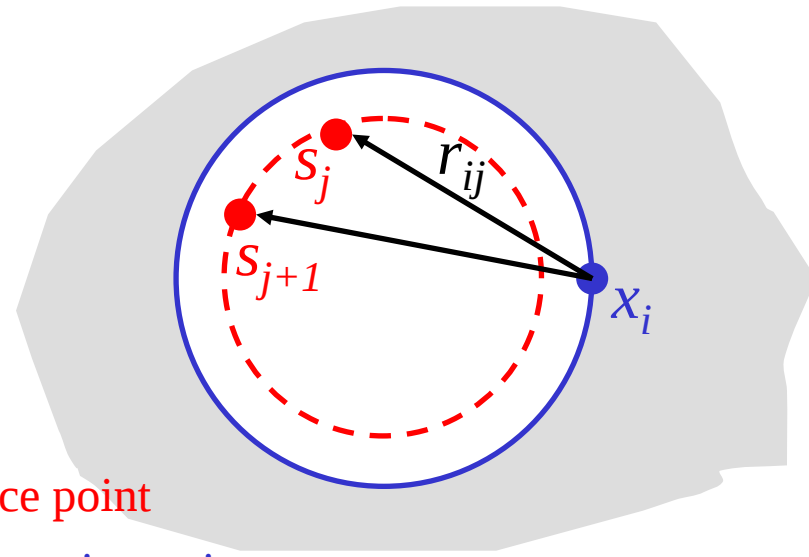




What happens in MFS ?



Interior problem



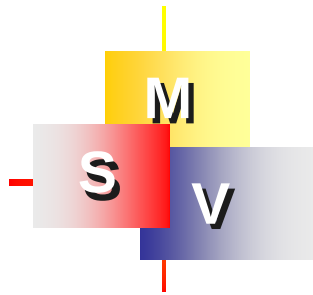
Exterior problem

● Source point
● Observation point

Field representation:
$$u(x_i) = \sum_j c_j \psi(s_j, x_i)$$

$$\psi(s_j, x_i) = \psi(r_{ij}), \quad r_{ij} \equiv |s_j - x_i|$$

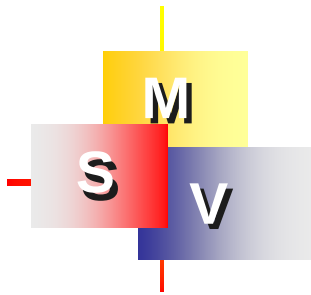




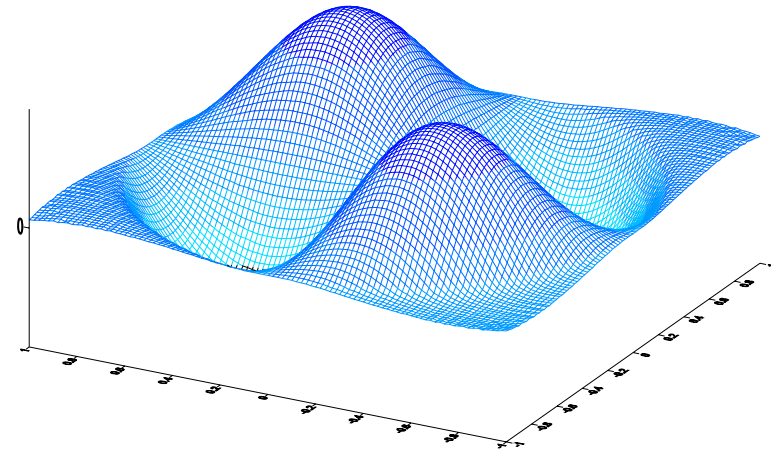
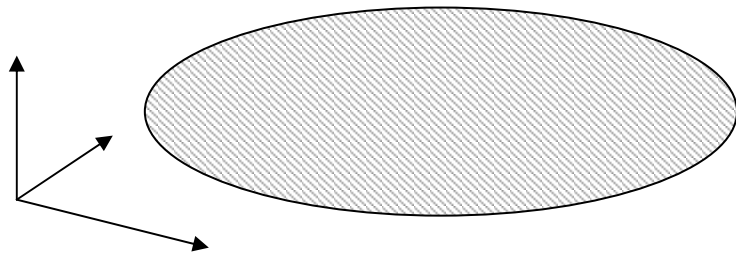
Outlines

1. Introduction
2. Problem statements
3. Mathematical analysis
4. Treatment methods
5. Numerical examples
6. Conclusions





Governing equation



Governing equation

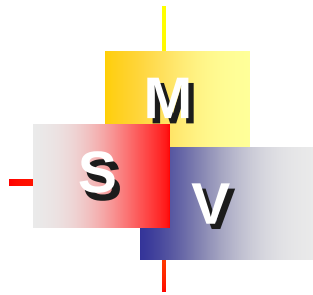
Membrane vibration

$$(\nabla^2 + k^2)u(x) = 0$$

Plate vibration

$$(\nabla^4 - \lambda^4)u(x) = 0$$





Fundamental solution

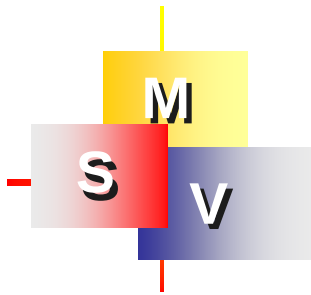
Membrane vibration

$$U(s, x) = iJ_0(kr) - Y_0(kr)$$

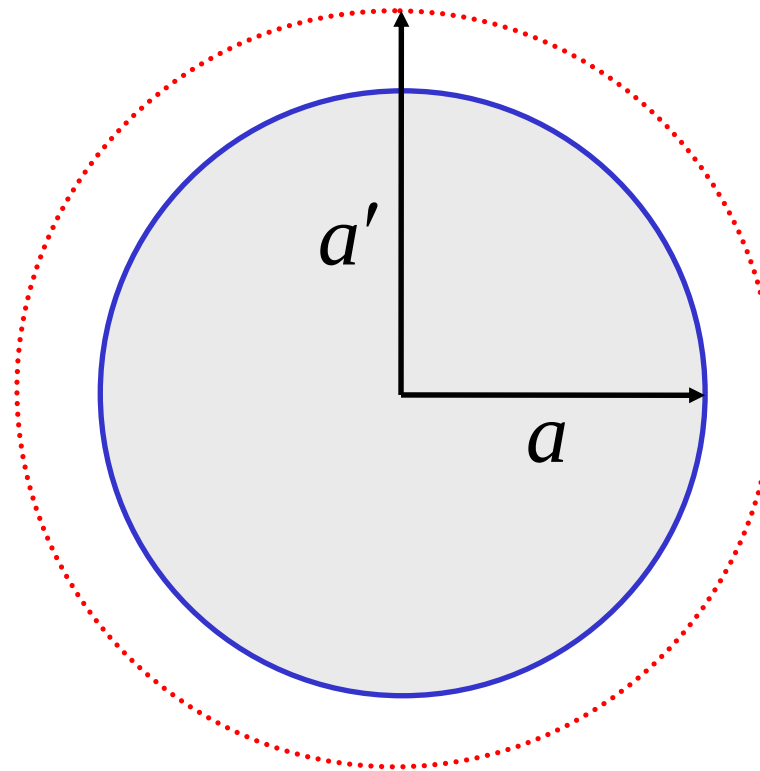
Plate vibration

$$U(s, x) = \frac{1}{8\lambda^2} \{ [Y_0(\lambda r) - iJ_0(\lambda r)] + \frac{2}{\pi} [K_0(\lambda r) - iI_0(\lambda r)] \}$$





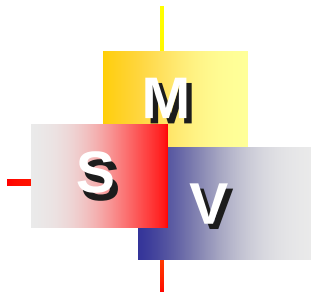
Simply-connected problem



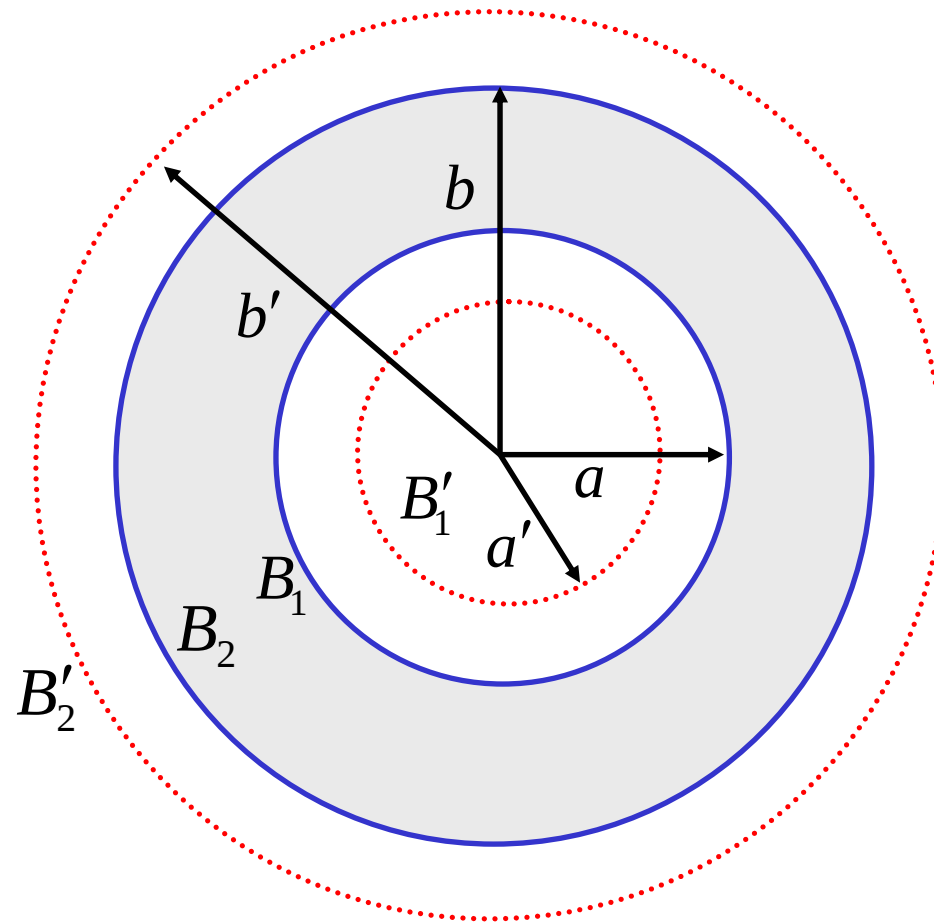
—— real boundary

..... fictitious boundary



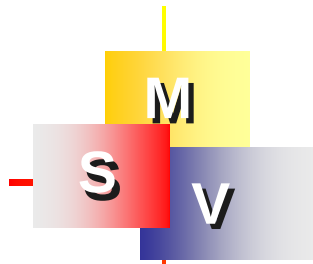


Multiply-connected problem



—— real boundary fictitious boundary





Two MFS for membrane problem

Single-layer potential approach

$$u(x_i) = \sum_j U(s_j, x_i) \phi_j$$

$$t(x_i) = \sum_j L(s_j, x_i) \phi_j$$

Double-layer potential approach

$$u(x_i) = \sum_j T(s_j, x_i) \psi_j$$

$$t(x_i) = \sum_j M(s_j, x_i) \psi_j$$

$$\begin{array}{ccc}
 U(s, x) & \xrightarrow{\frac{\partial}{\partial n_s}} & T(s, x) \\
 \frac{\partial}{\partial n_x} \downarrow & & \downarrow \frac{\partial}{\partial n_x} \\
 L(s, x) & \xrightarrow{\frac{\partial}{\partial n_s}} & M(s, x)
 \end{array}$$

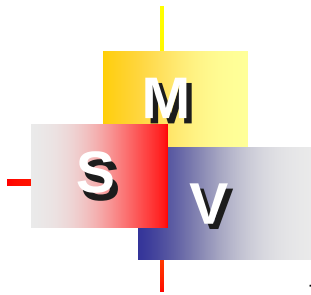
ASME, App. Mech. Rev.
(Chen and Hong, 1999)



ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 10

Department of Harbor and River Engineering, Nation Taiwan Ocean University





Kernel functions of plate vibration

$U(s, x)$ = Fundamental solution

Slope operator

$$\Theta(s, x) = K_{\theta, s}(U(s, x)) = \frac{\partial U(s, x)}{\partial n_s}$$

Moment operator

$$M(s, x) = K_{m, s}(U(s, x))$$

$$= \nu \nabla_s^2 U(s, x) + (1 - \nu) \frac{\partial^2 U(s, x)}{\partial n_s^2}$$

Shear operator

$$V(s, x) = K_{v, s}(U(s, x))$$

$$= \frac{\partial \nabla_s^2 U(s, x)}{\partial n_s} + (1 - \nu) \frac{\partial}{\partial t_s} \left(\frac{\partial^2 U(s, x)}{\partial n_s \partial t_s} \right)$$



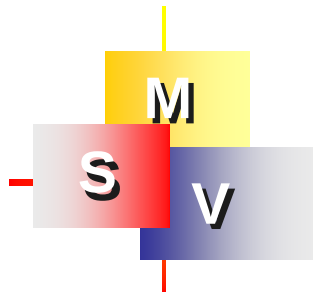


Plate problem

Selected two from four (U, Θ, M and V) (C_2^4 options)

Displacement

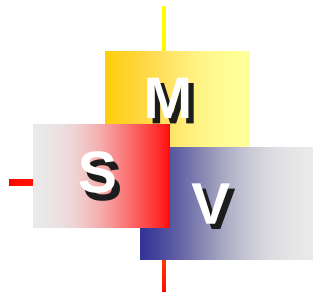
$$u(x) = \sum_{j=1}^{2N} P(s_j, x) \phi(s_j) + \sum_{j=1}^{2N} Q(s_j, x) \psi(s_j)$$

Slope $\theta(x) = K_{\theta, x}(u(x))$

Moment $m(x) = K_{m, x}(u(x))$

Shear $v(x) = K_{v, x}(u(x))$





Matrix form

Membrane

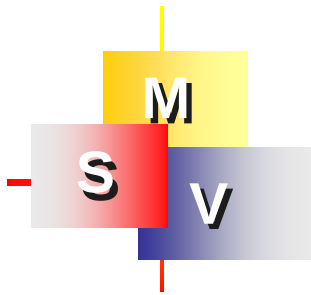
$$\{u\} = [U]\{\phi\} \quad \text{Dirichlet problem}$$

$$\{t\} = [L]\{\phi\} \quad \text{Neumann problem}$$

Plate

Clamped	$\rightarrow$ $\rightarrow$	$\{u\} = [P]\{\phi\} + [Q]\{\psi\}$	$\leftarrow$ $\leftarrow$	Simply-supported
		$\{\theta\} = [P_\theta]\{\phi\} + [Q_\theta]\{\psi\}$		
Free	$\rightarrow$ $\rightarrow$	$\{m\} = [P_m]\{\phi\} + [Q_m]\{\psi\}$	$\leftarrow$ $\leftarrow$	
		$\{v\} = [P_v]\{\phi\} + [Q_v]\{\psi\}$		

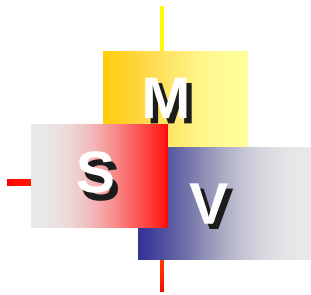




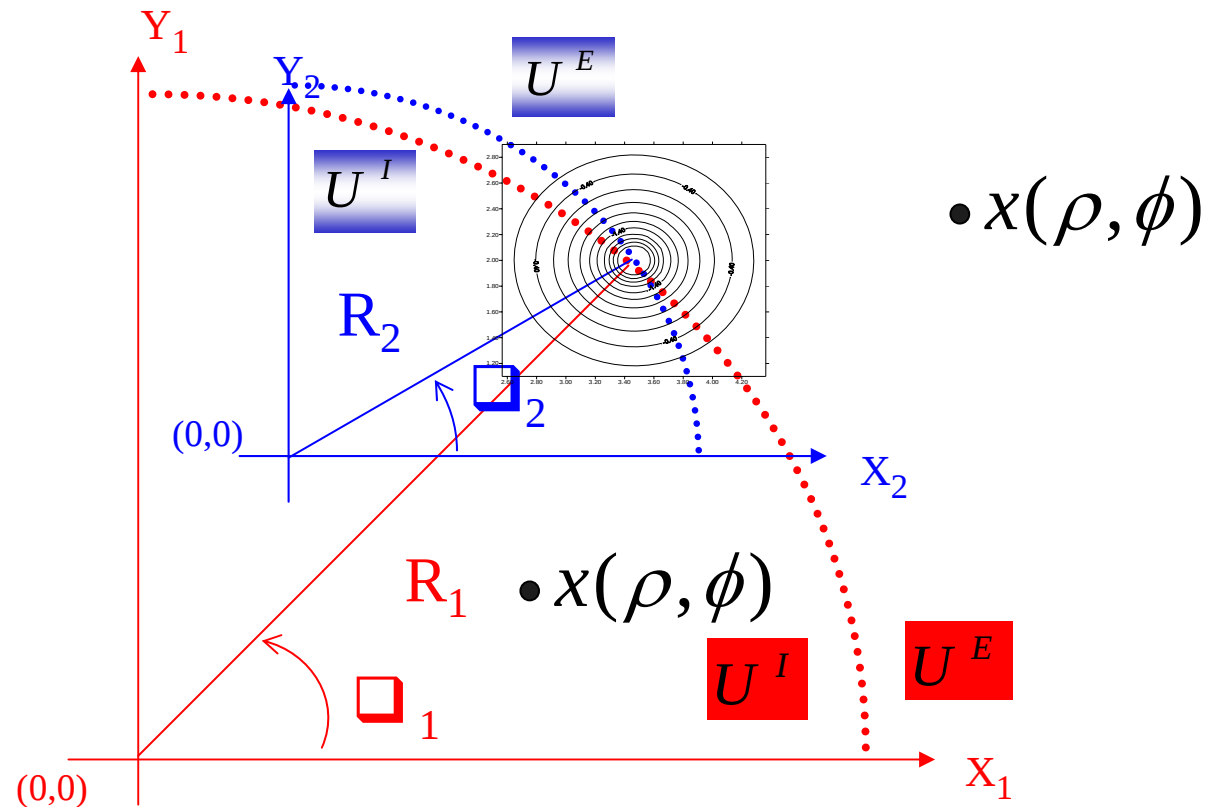
Outlines

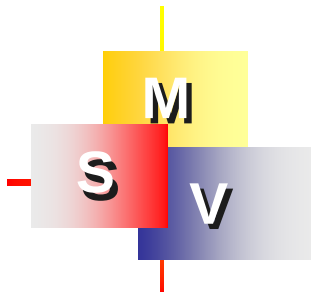
1. Introduction
2. Problem statements
- 3. Mathematical analysis**
4. Treatment methods
5. Numerical examples
6. Conclusions





Degenerate kernel





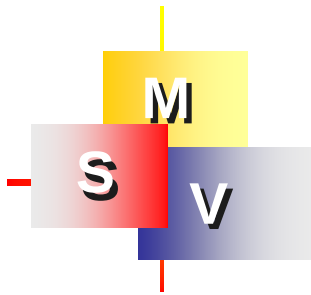
Circulant

Uniform discretization into $2N$ nodes on the circular boundary

$$[U] = \begin{bmatrix} a_0 & a_1 & a_2 & \cdots & a_{2N-2} & a_{2N-1} \\ a_{2N-1} & a_0 & a_1 & \cdots & a_{2N-3} & a_{2N-2} \\ a_{2N-2} & a_{2N-1} & a_0 & \cdots & a_{2N-4} & a_{2N-3} \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ a_2 & a_3 & a_4 & \cdots & a_0 & a_1 \\ a_1 & a_2 & a_3 & \cdots & a_{2N-1} & a_0 \end{bmatrix}$$

$$[U] = a_0 I + a_1 C_{2N} + a_2 (C_{2N})^2 + \cdots + a_{2N-1} (C_{2N})^{2N-1}$$





Circulant

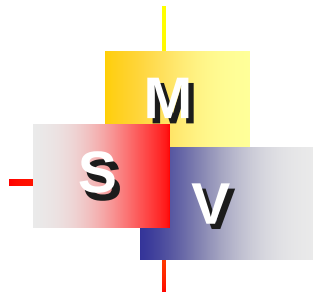
$$C_{2N} = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 & 0 \\ 0 & 0 & 1 & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & 0 & 1 \\ 1 & 0 & 0 & \cdots & 0 & 0 \end{bmatrix}_{2N \times 2N}$$

$$\alpha_\ell = e^{i\frac{2\pi\ell}{2N}} = \cos\left(\frac{2\pi\ell}{2N}\right) + i \sin\left(\frac{2\pi\ell}{2N}\right) \quad : \text{eigenvalue of } C_{2N}$$

Membrane: $\lambda_\ell = 2NJ_\ell(ka)[iJ_\ell(ka') - Y_\ell(ka')]$

Plate: $\lambda_\ell^{[U]} = \frac{N}{4\lambda^2} \{ J_m(\lambda\rho)[Y_m(\lambda R) - iJ_m(\lambda R)] + \frac{2}{\pi}(-1)^m I_m(\lambda\rho)[(-1)^m K_m(\lambda R) - iI_m(\lambda R)] \}$





Singular Value Decomposition

$$[U] = \Phi \Sigma_{[U]} \Phi^H$$

$$= \Phi \begin{bmatrix} \lambda_0^{[U]} & 0 & 0 & \dots & 0 & 0 & 0 \\ 0 & \lambda_1^{[U]} & 0 & \dots & 0 & 0 & 0 \\ 0 & 0 & \lambda_{-1}^{[U]} & \dots & 0 & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & \dots & \lambda_{(N-1)}^{[U]} & 0 & 0 \\ 0 & 0 & 0 & \dots & 0 & \lambda_{-(N-1)}^{[U]} & 0 \\ 0 & 0 & 0 & \dots & 0 & 0 & \lambda_N^{[U]} \end{bmatrix}_{2N \times 2N} \Phi^H$$

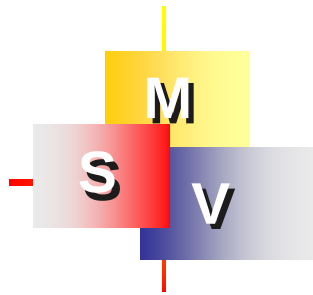
H is transpose and conjugate



ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 18

Department of Harbor and River Engineering, Nation Taiwan Ocean University

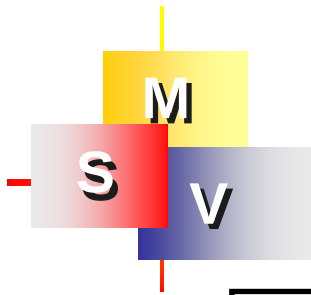




Outlines

1. Introduction
2. Problem statements
3. Mathematical analysis
- 4. Treatment methods**
5. Numerical examples
6. Conclusions

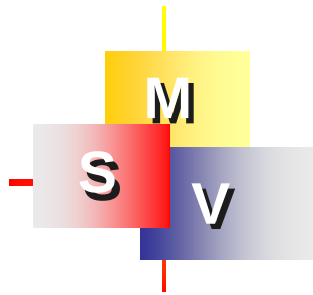




Methods of extracting true and spurious eigenvalues

SVD updating document	$[C_R] = [U_R T_R]^T$	Extraction true
Burton & Miller method	$[[U_R] + i[T_R]] \{\varphi\} = \{0\}$	Extraction true
SVD updating term	$[P_R] = \begin{bmatrix} U_R \\ L_R \end{bmatrix}$	Extraction spurious





Outlines

1. Introduction
2. Problem statements
3. Mathematical analysis
4. Treatment methods
- 5. Numerical examples**
6. Conclusions

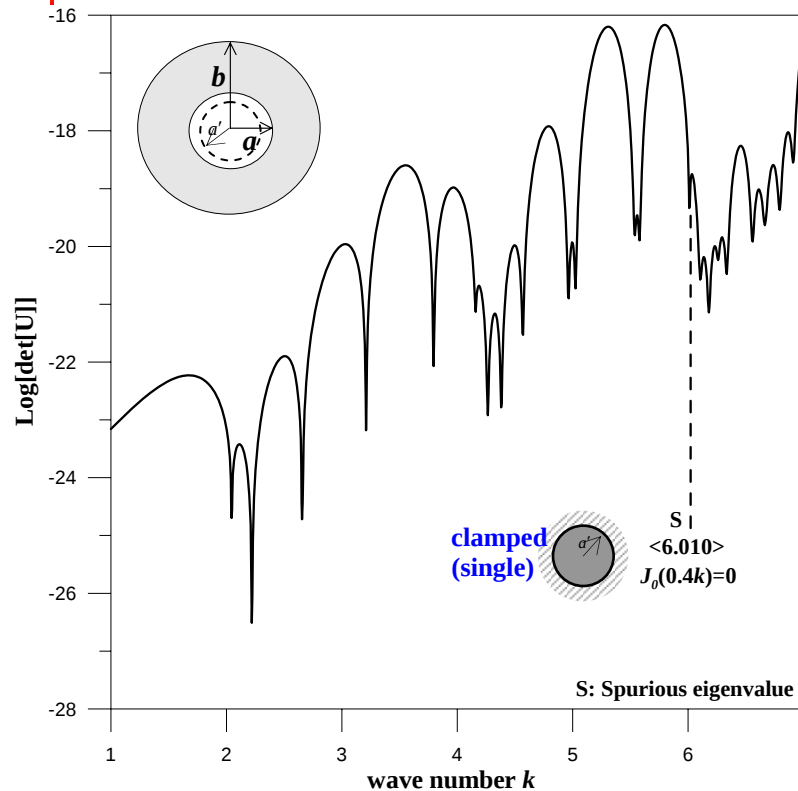


M

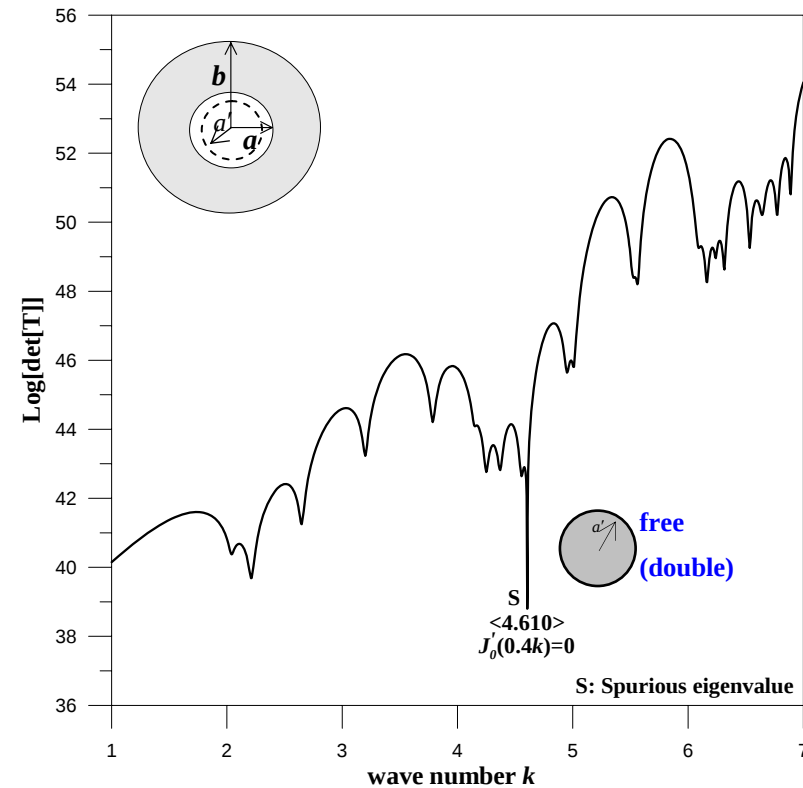
S

V

Clamped-clamped problem (membrane)



Single-layer potential approach



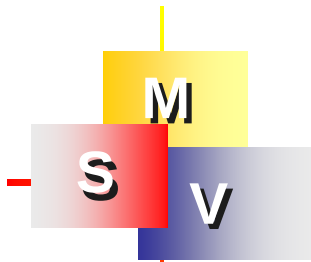
Double-layer potential approach



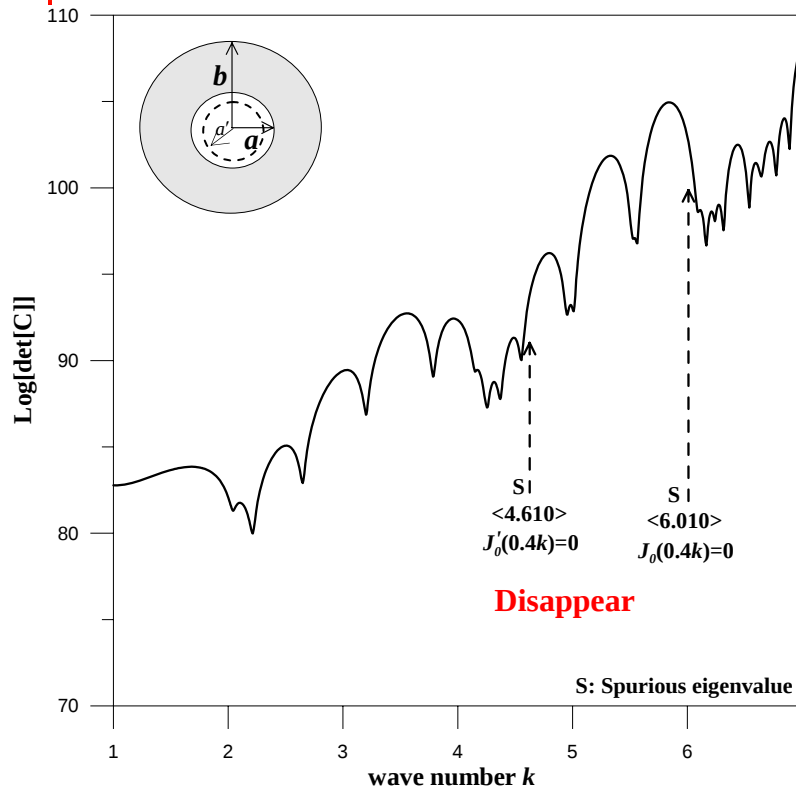
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 22

Department of Harbor and River Engineering, Nation Taiwan Ocean University



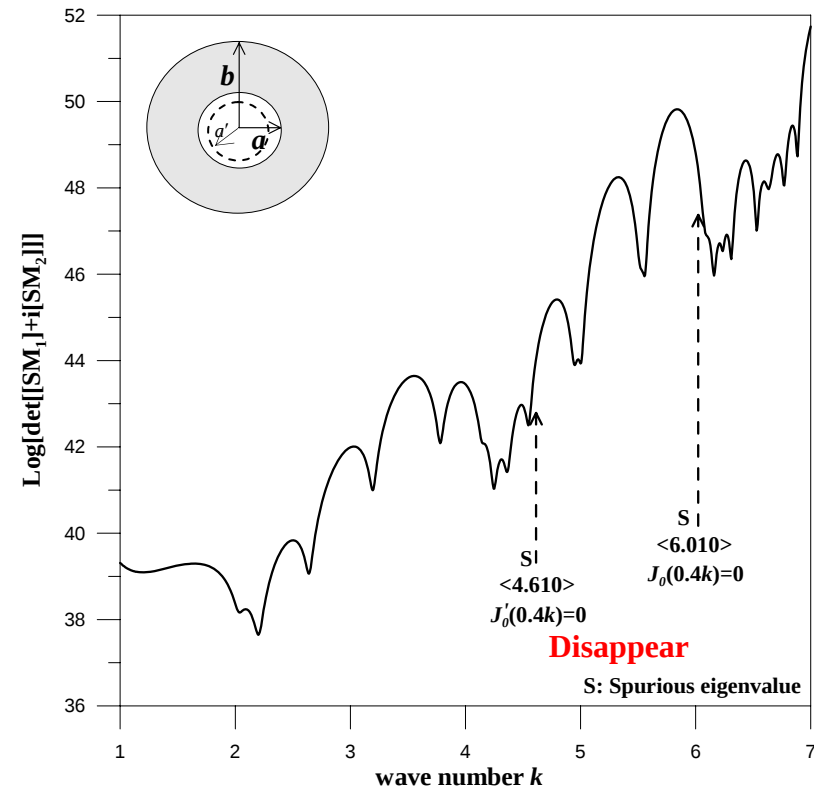


Clamped-clamped problem (membrane)



Single-layer potential approach

+ SVD updating document



Single-layer potential approach

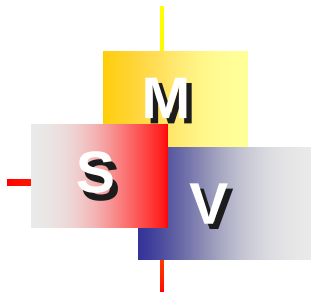
+ Burton & Miller method



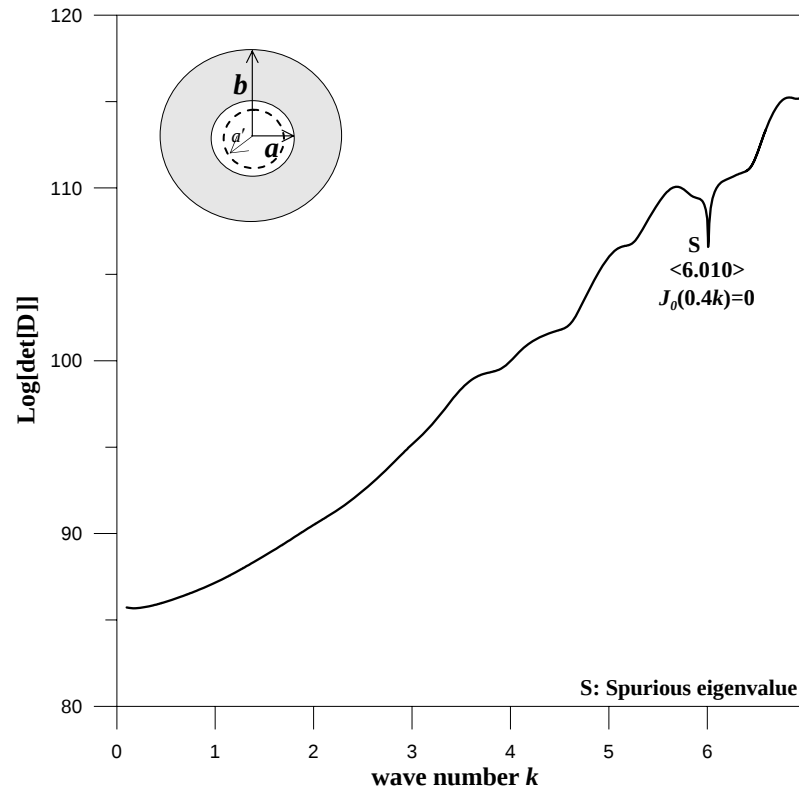
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 23

Department of Harbor and River Engineering, Nation Taiwan Ocean University





Clamped-clamped problem (membrane)



Single-layer potential approach

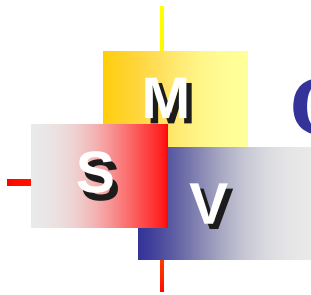
+ SVD updating term



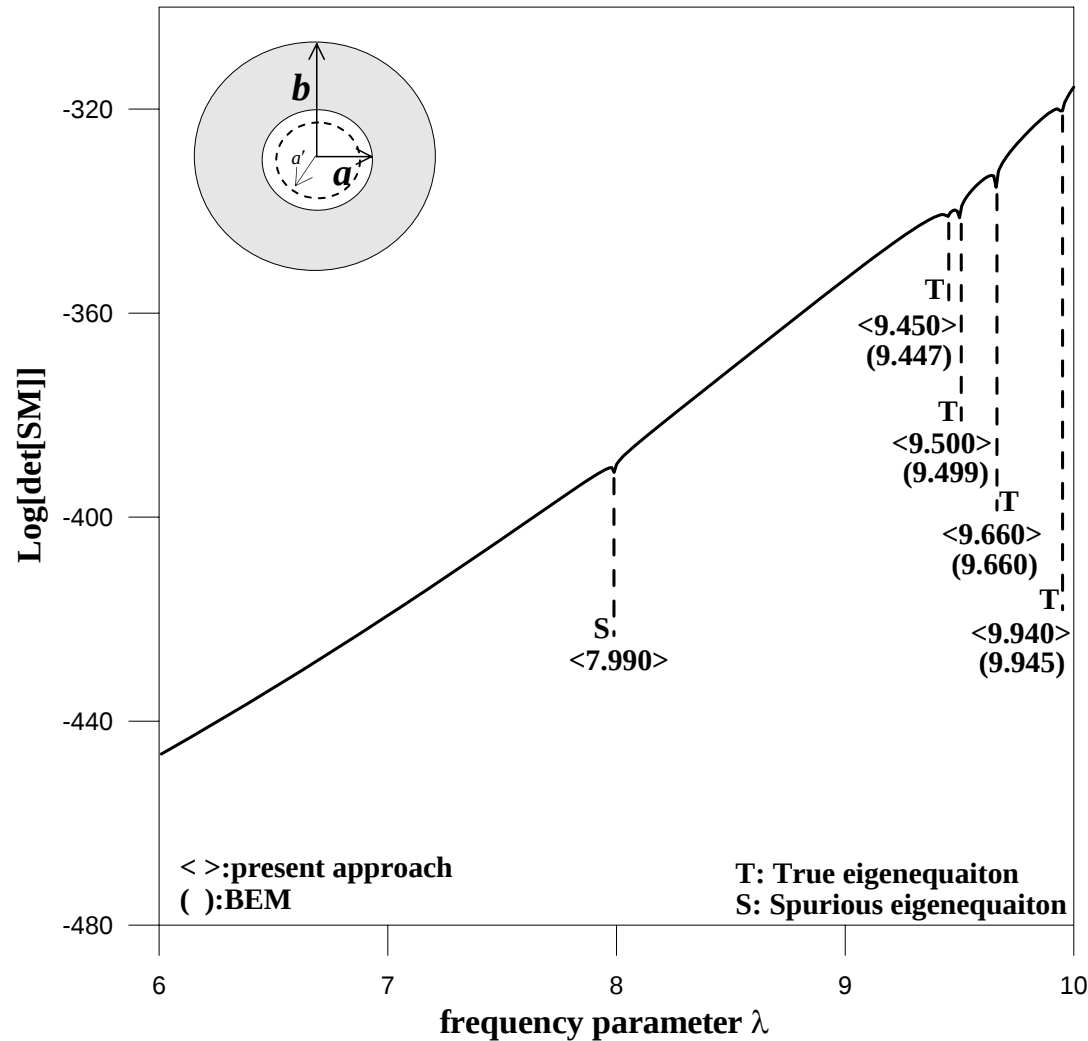
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 24

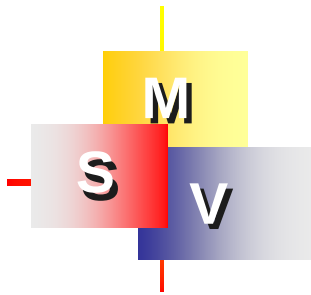
Department of Harbor and River Engineering, Nation Taiwan Ocean University



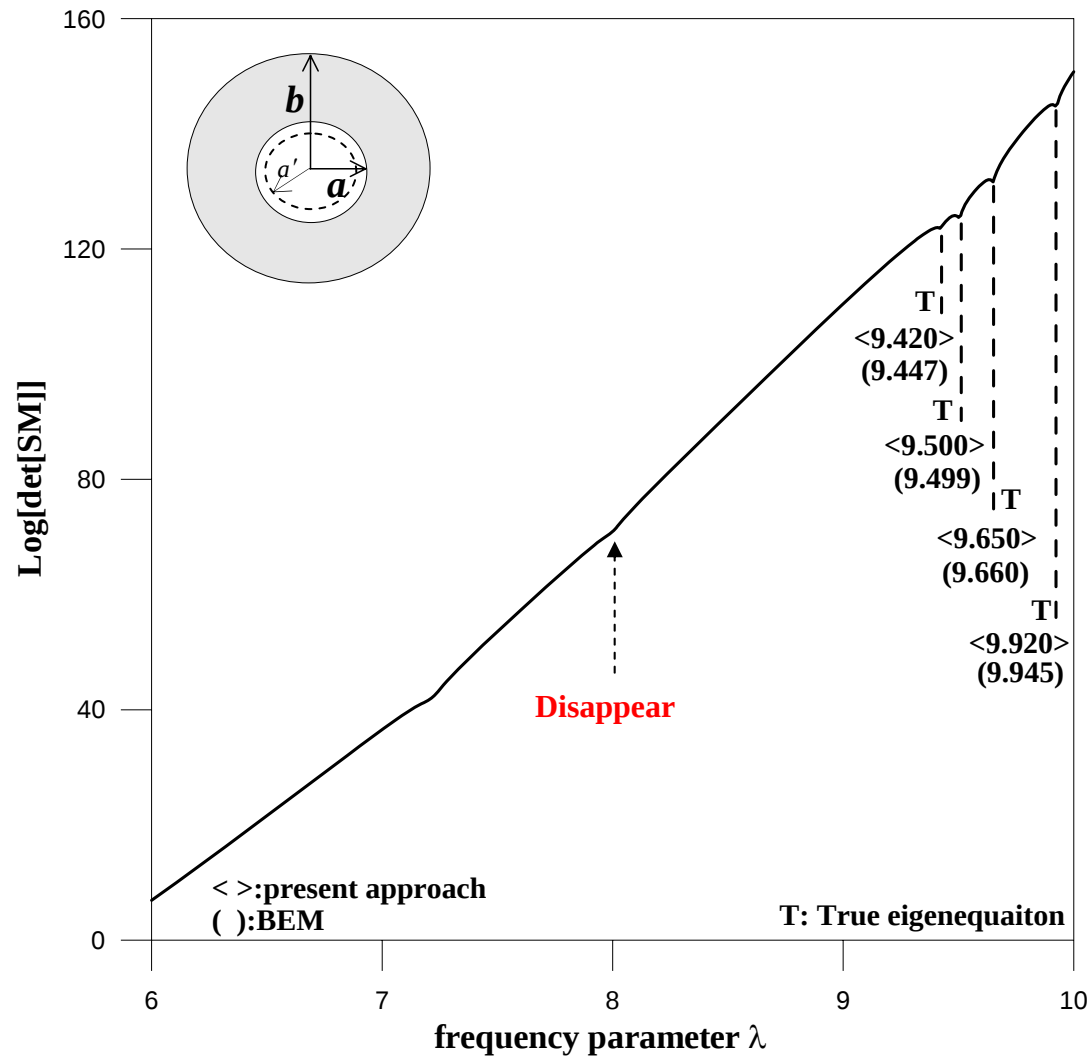


Clamped-clamped plate ($U-\theta$ formulation)





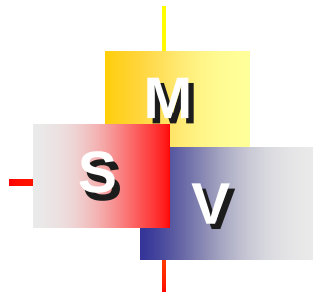
Burton & Miller method



ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 26

Department of Harbor and River Engineering, Nation Taiwan Ocean University

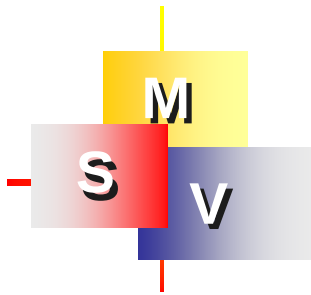




Outlines

1. Introduction
2. Problem statements
3. Mathematical analysis
4. Treatment methods
5. Numerical examples
- 6. Conclusions**

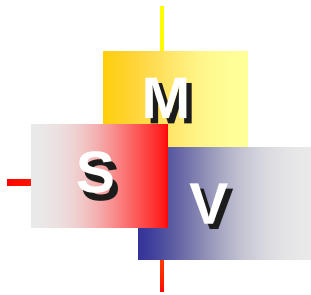




Conclusions

1. We have verified that the **true eigenequation depends on the boundary condition** while **spurious eigenequation** is embedded in each formulation.
2. The spurious eigenvalues occurring in the multiply-connected eigenproblem for membrane and plate are the **true eigenvalues of the associated problem bounded** by the **inner fictitious boundary** where the sources are distributed.
3. Three remedies, the **SVD updating document**, the **SVD updating term** and the **Burton & Miller method**, were successfully employed to suppress the appearance of the spurious eigenvalues





The End

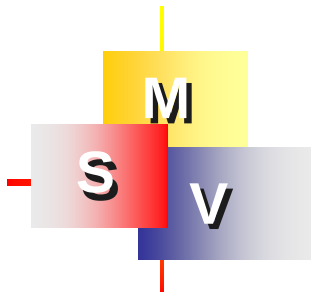
Thanks for your kind attention

<http://ind.ntou.edu.tw/~msvlab/>

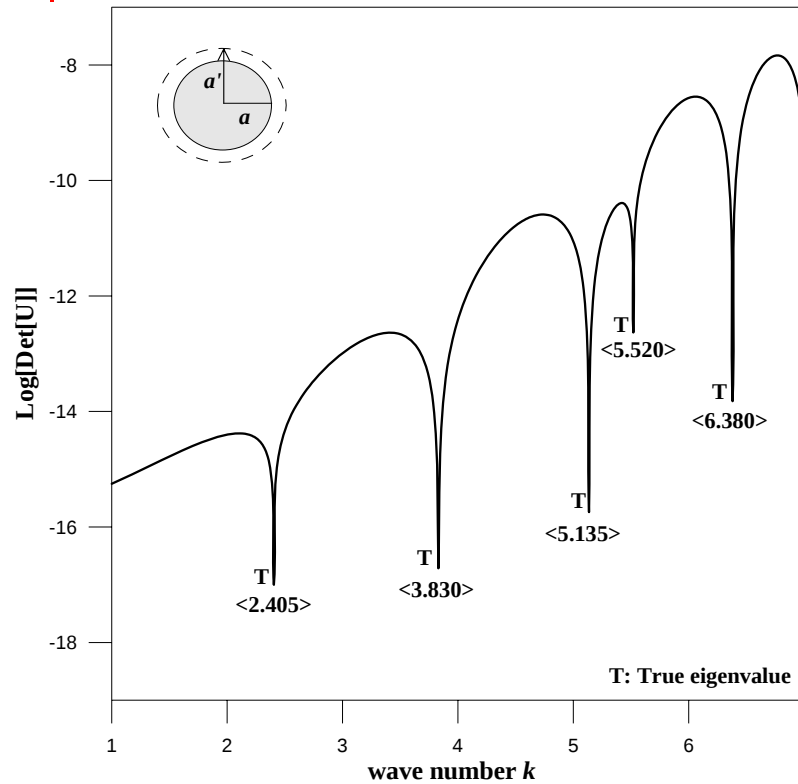


ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 29
Department of Harbor and River Engineering, Nation Taiwan Ocean University

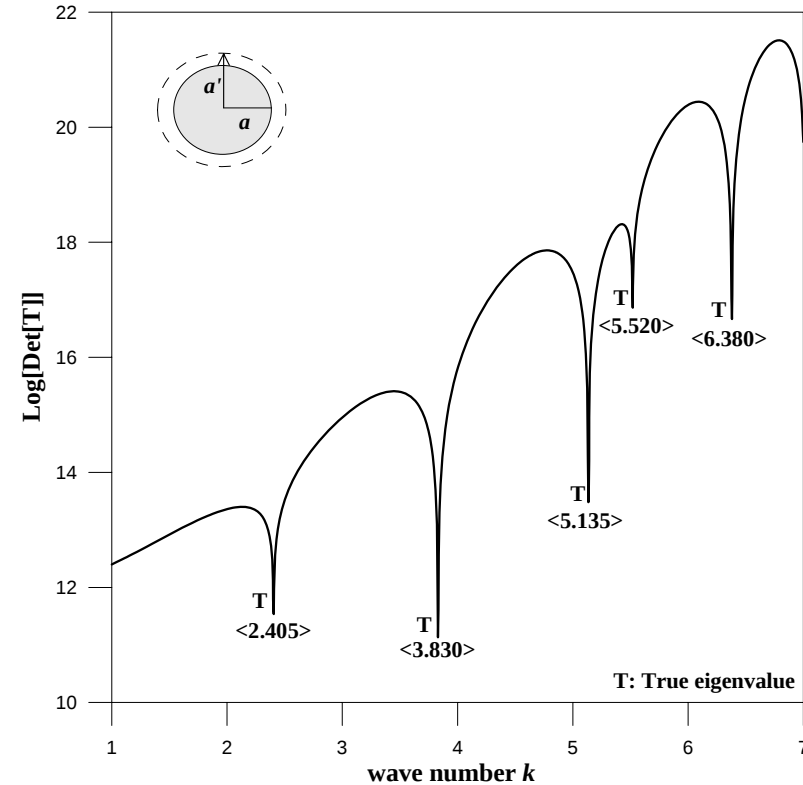




Dirichlet problem (Complex-valued MFS)



Single-layer potential approach



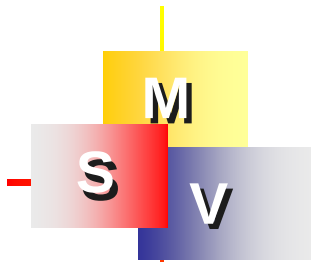
Double-layer potential approach



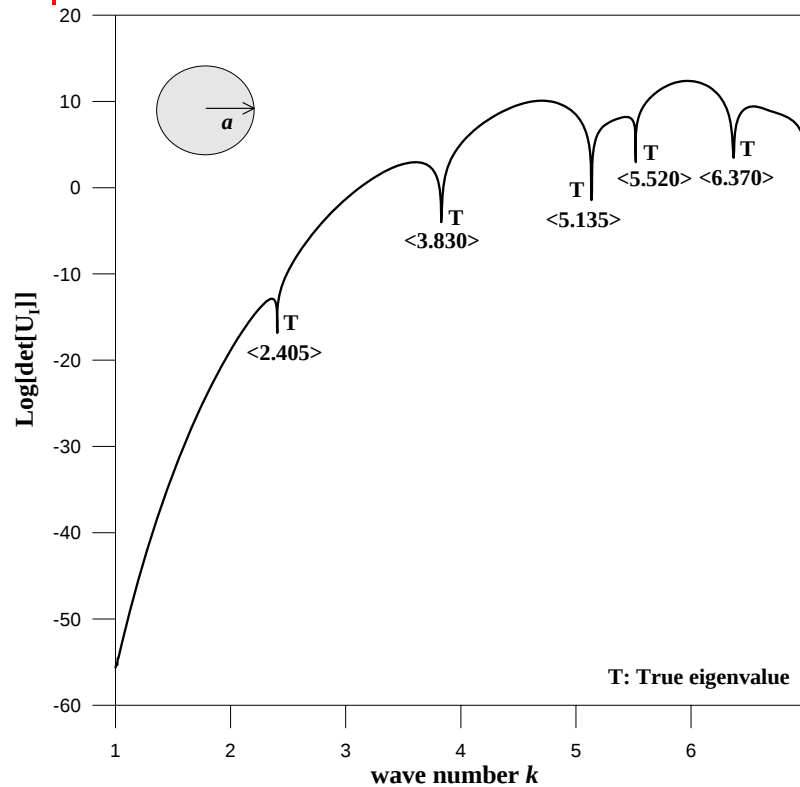
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 30

Department of Harbor and River Engineering, Nation Taiwan Ocean University

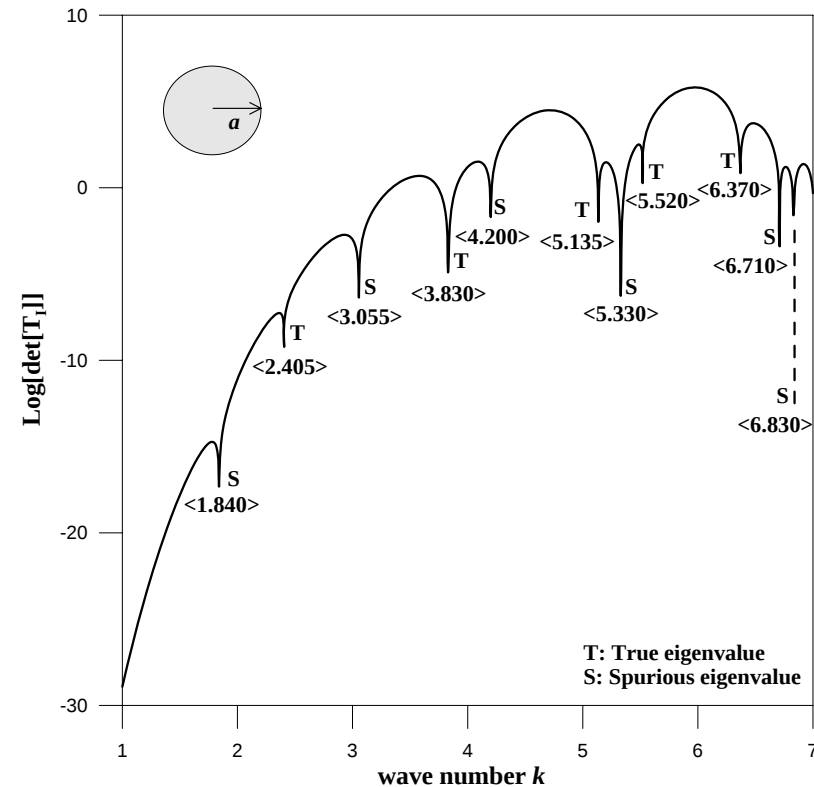




Dirichlet problem (Imaginary-part MFS)



Single-layer potential approach



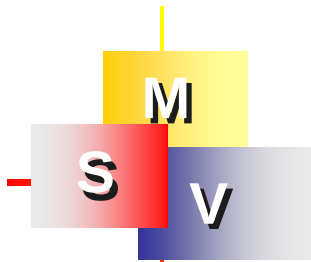
Double-layer potential approach



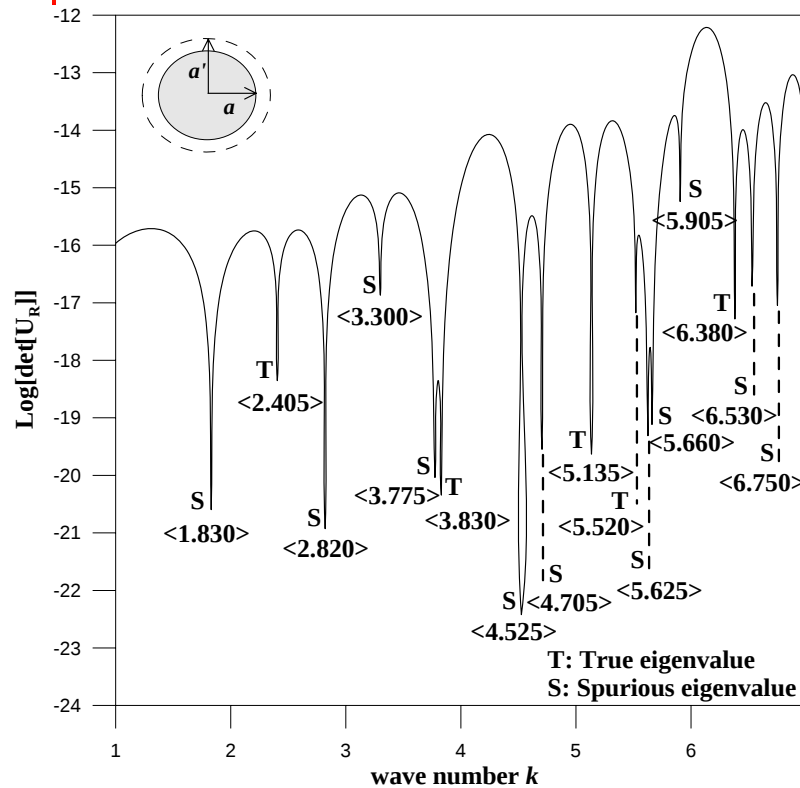
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 31

Department of Harbor and River Engineering, Nation Taiwan Ocean University

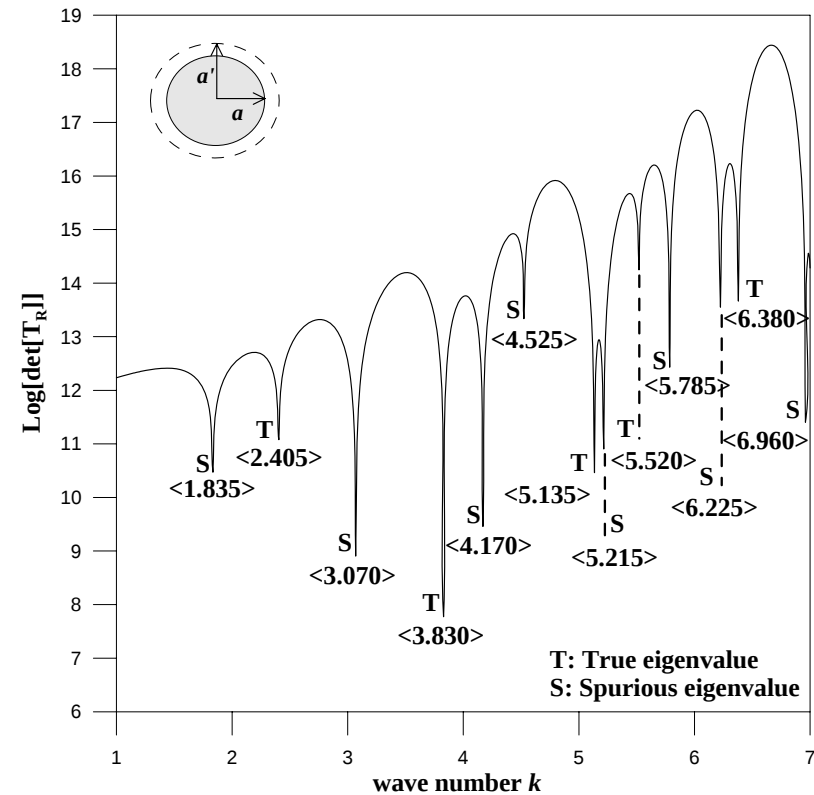




Dirichlet problem (Real-part MFS)



Single-layer potential approach



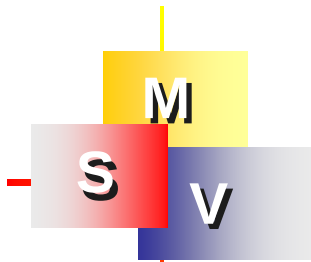
Double-layer potential approach



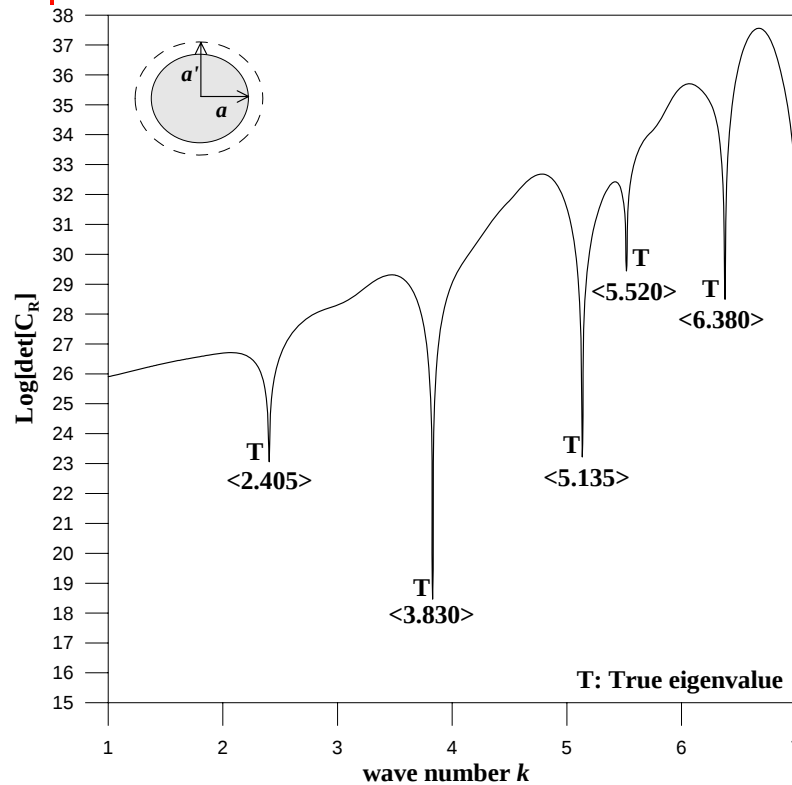
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 32

Department of Harbor and River Engineering, Nation Taiwan Ocean University

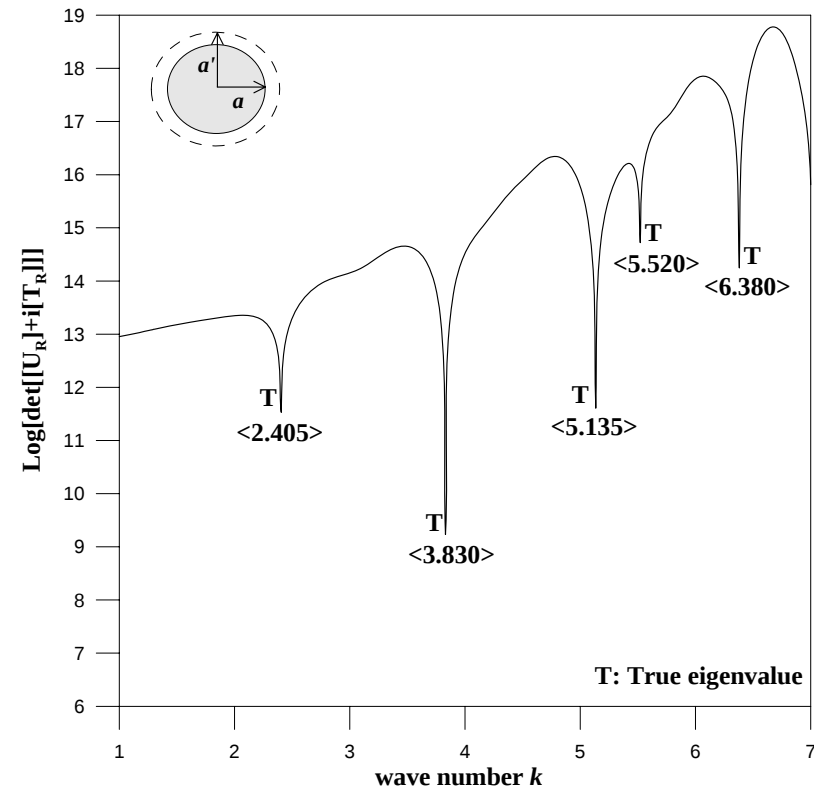




Dirichlet problem (Real-part MFS)



Single-layer potential approach
+SVD updating document

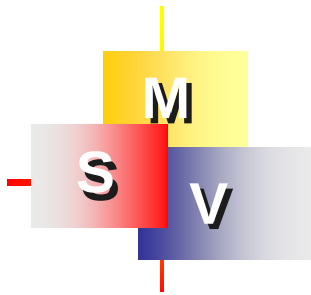


Single-layer potential approach
+Burton & Miller method

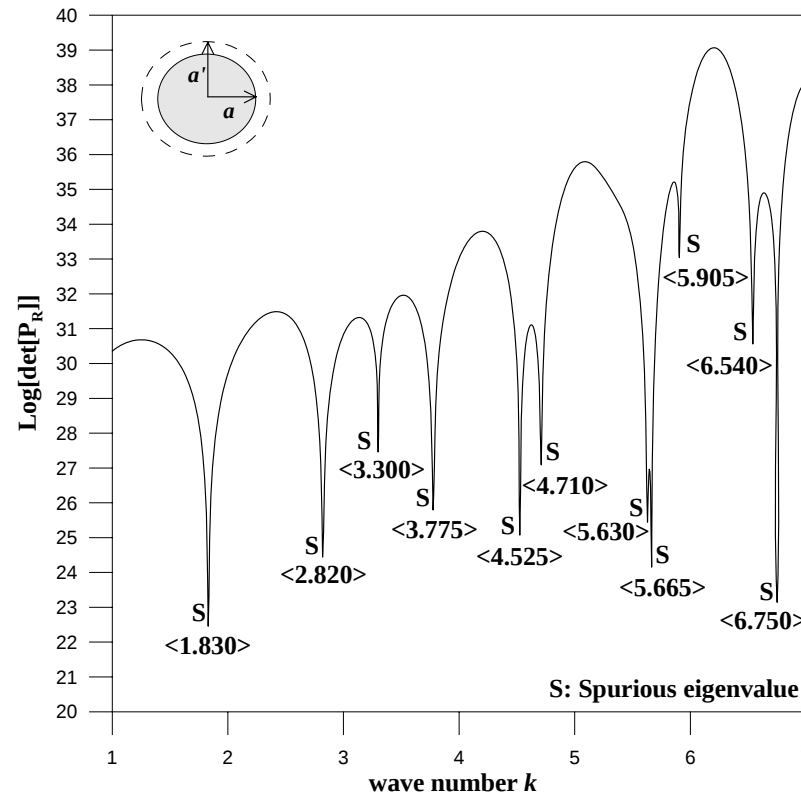


ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 33
Department of Harbor and River Engineering, Nation Taiwan Ocean University



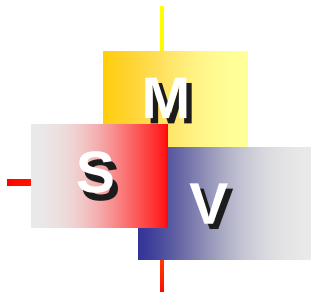


Dirichlet problem (Real-part MFS)

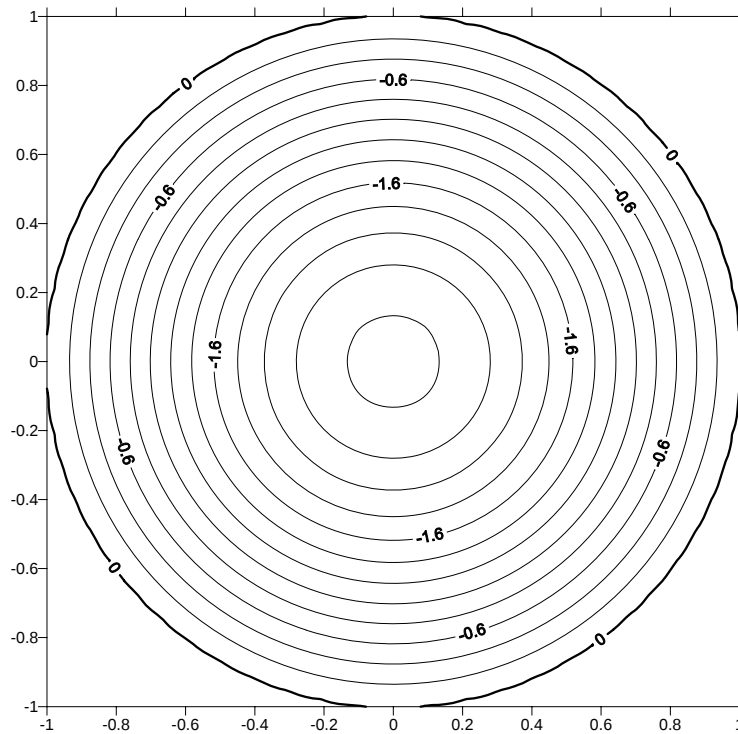


Single-layer potential approach
+SVD updating term

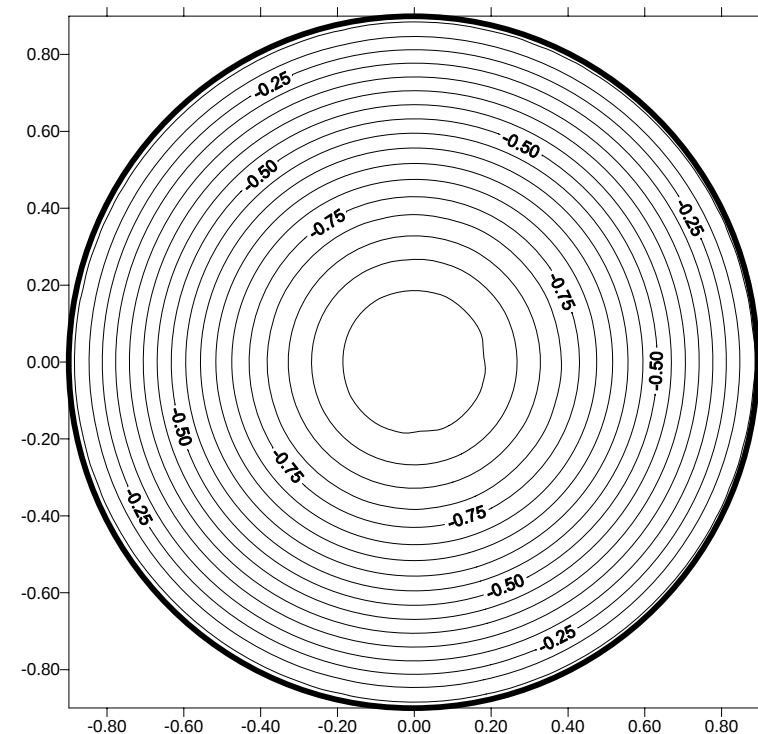




Mode 1 ($k_1=2.045$)



Present method



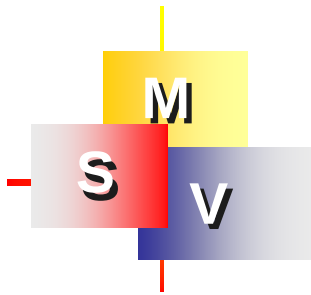
Analytical solution



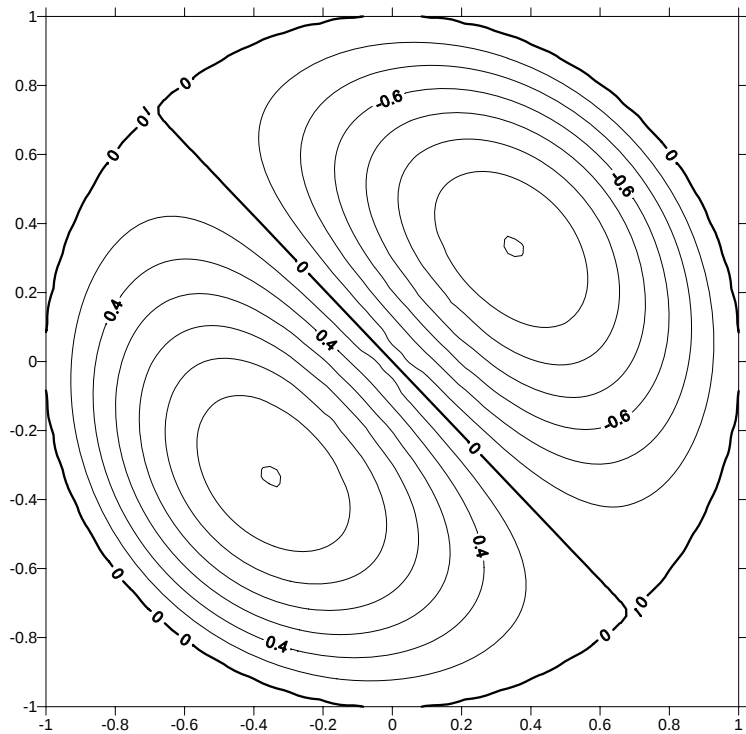
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 35

Department of Harbor and River Engineering, Nation Taiwan Ocean University

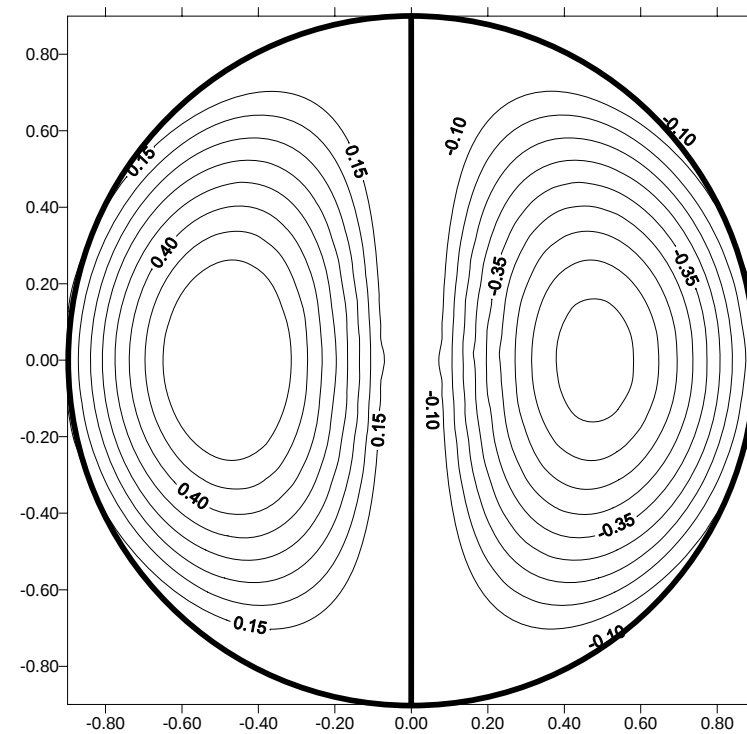




Mode 2 ($k_2=3.083$)



Present method



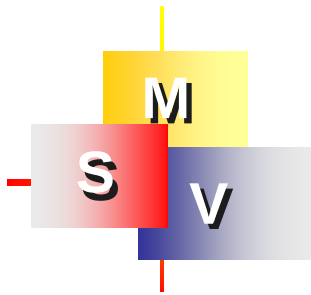
Analytical solution



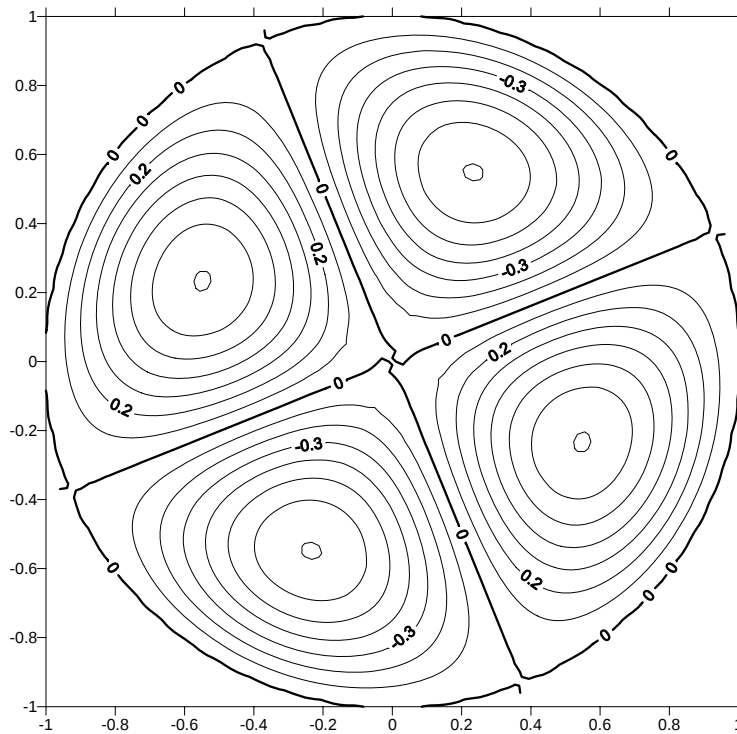
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 36

Department of Harbor and River Engineering, Nation Taiwan Ocean University

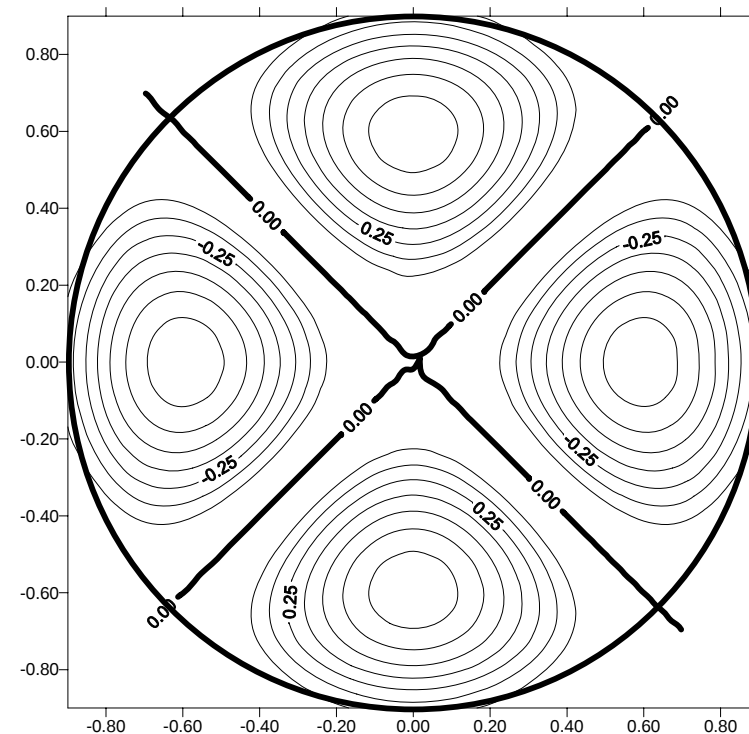




Mode 3 ($k_3=5.135$)

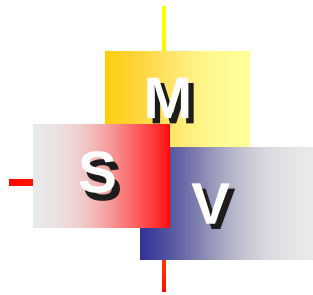


Present method

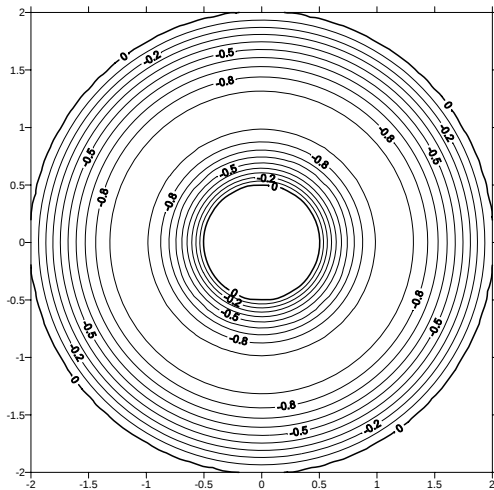


Analytical solution

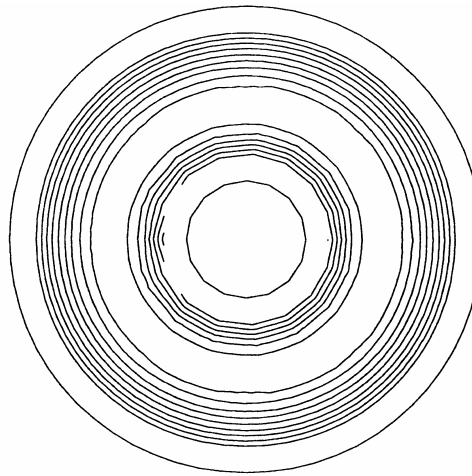




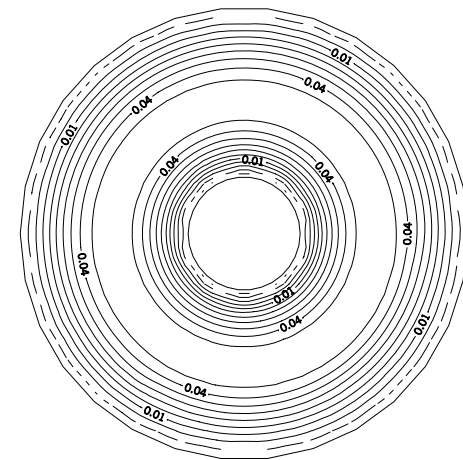
Mode 1 ($k_1=2.05$)



Present method

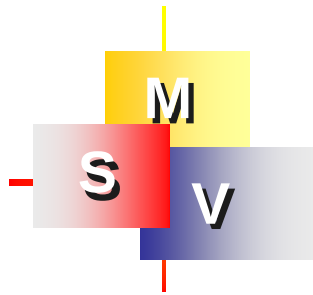


FEM

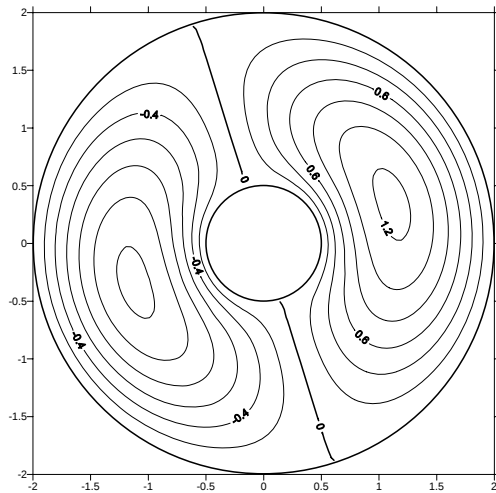


BEM

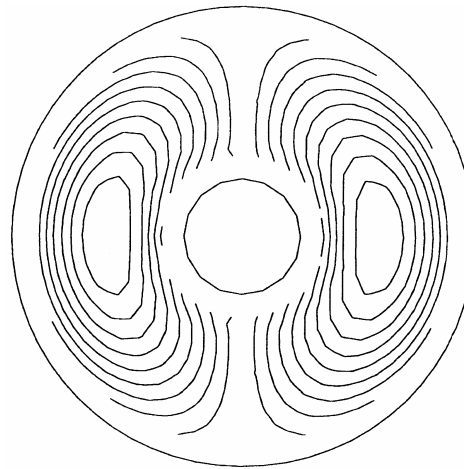




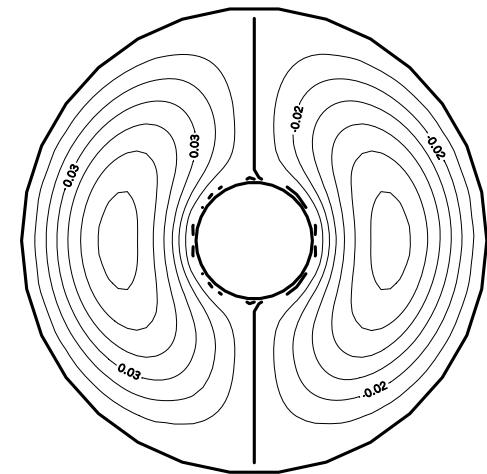
Mode 2 ($k_2=2.23$)



Present method

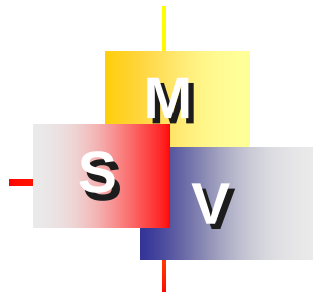


FEM

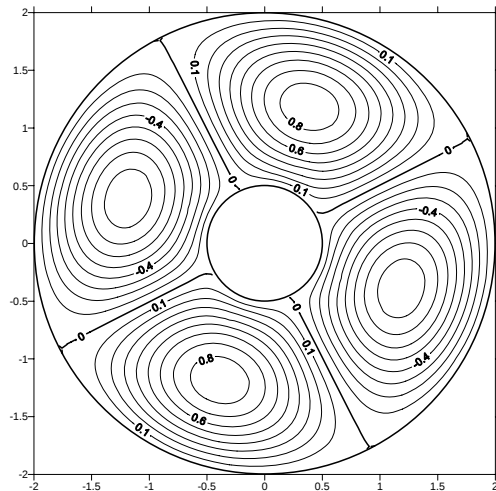


BEM

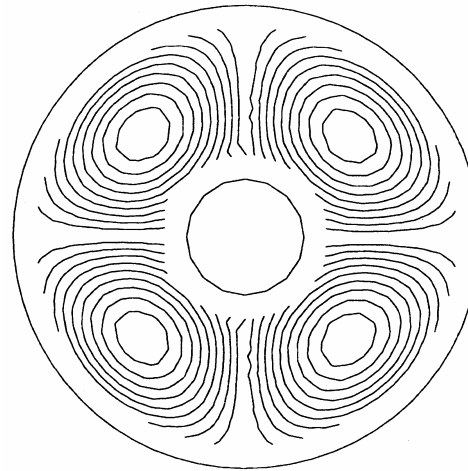




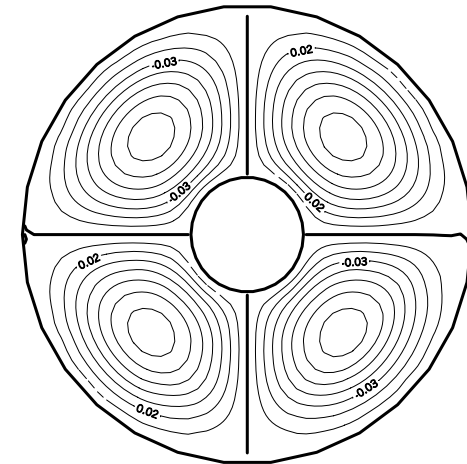
Mode 3 ($k_3=2.66$)



Present method

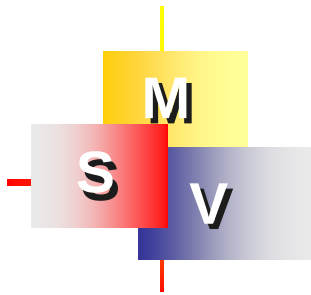


FEM

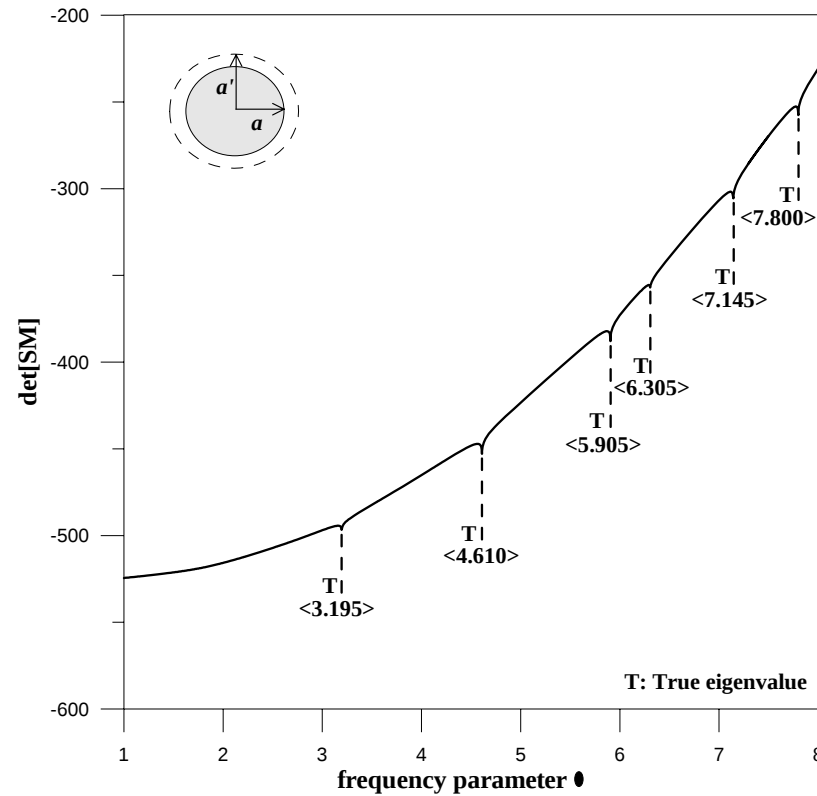


BEM



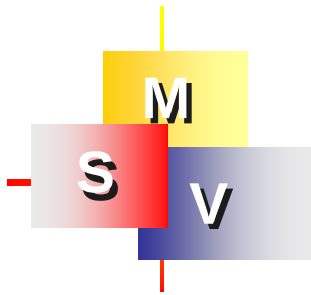


Clamped plate

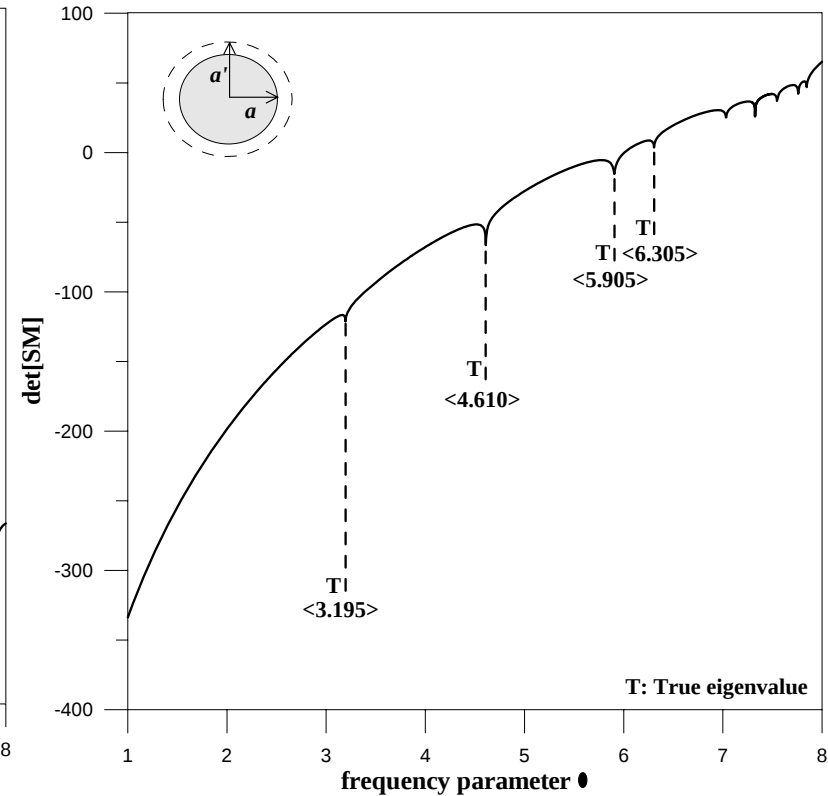
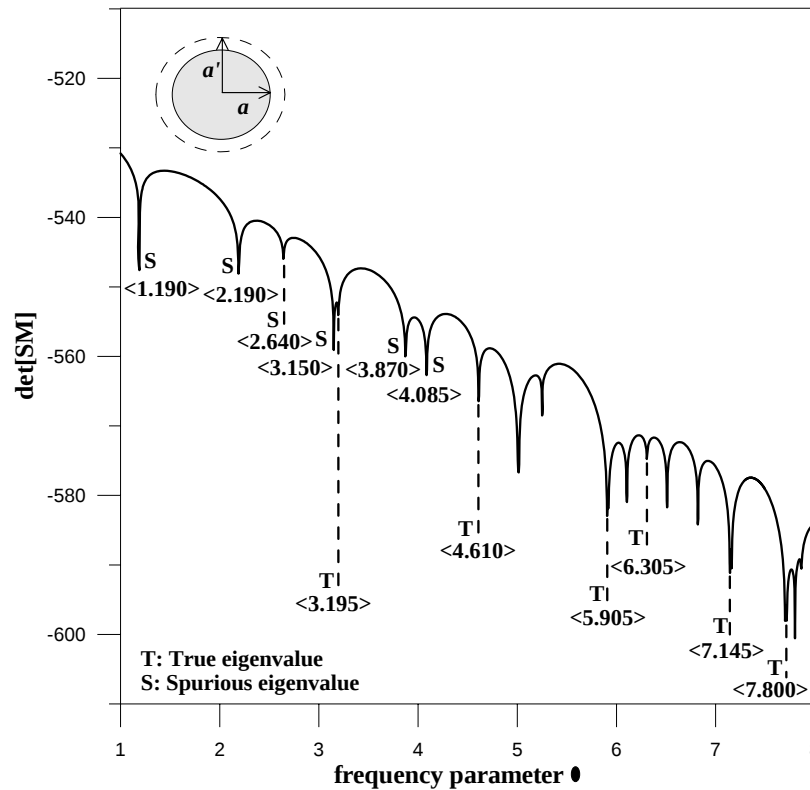


Complex-valued MFS





Clamped plate



Real-part MFS

Imaginary-part MFS



ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 42

Department of Harbor and River Engineering, Nation Taiwan Ocean University

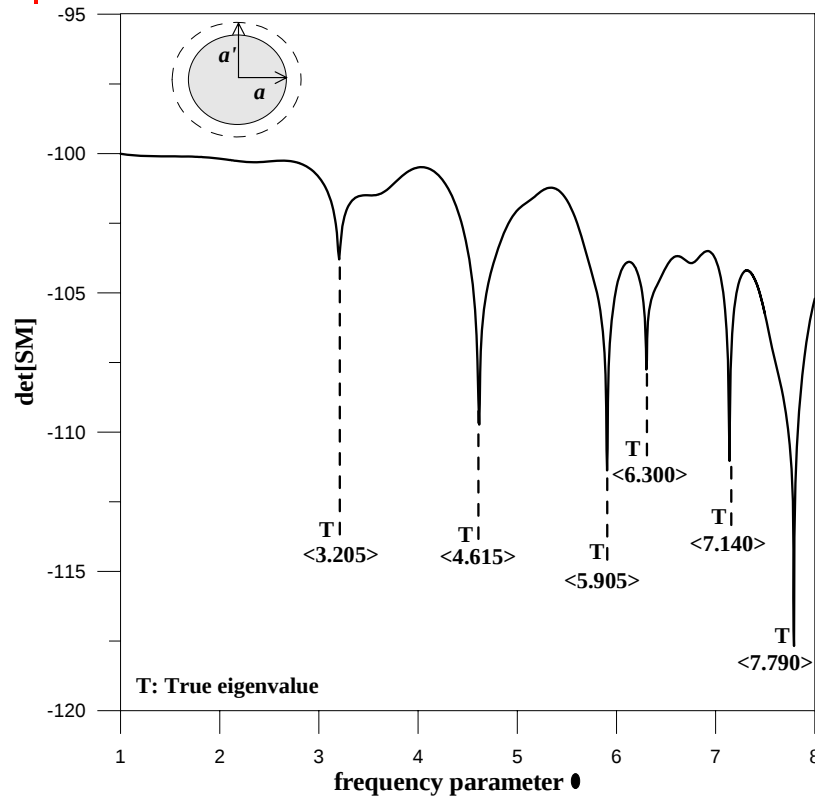


M

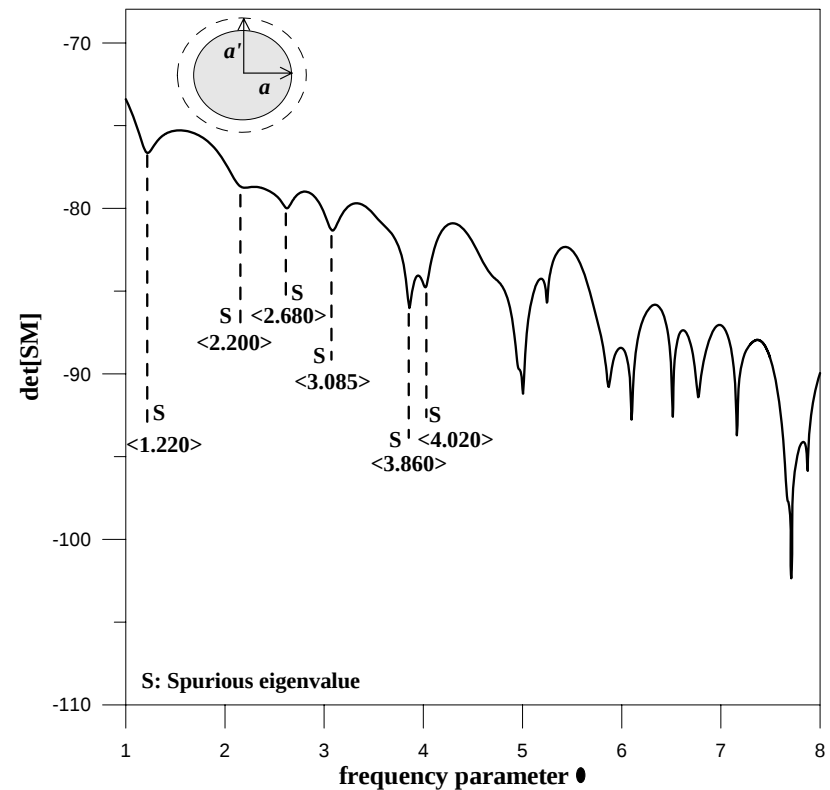
S

V

Clamped plate



Real-part MFS +SVD
updating document



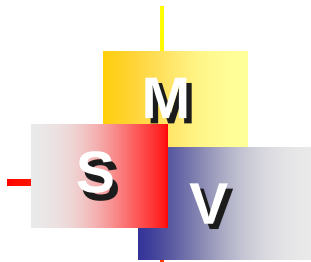
Real-part MFS
+SVD updating term



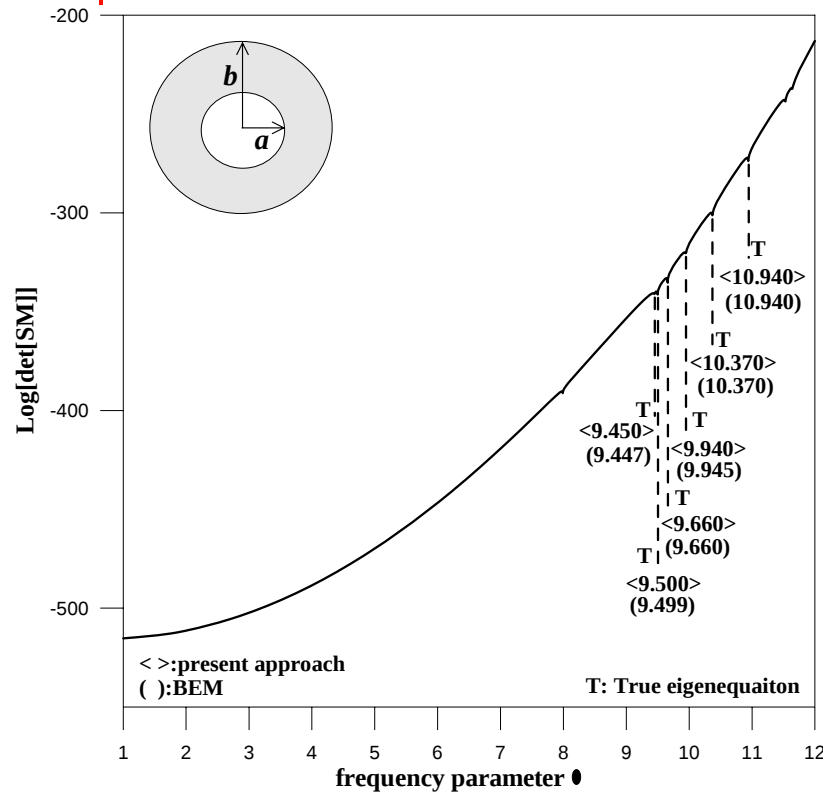
ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 43

Department of Harbor and River Engineering, Nation Taiwan Ocean University

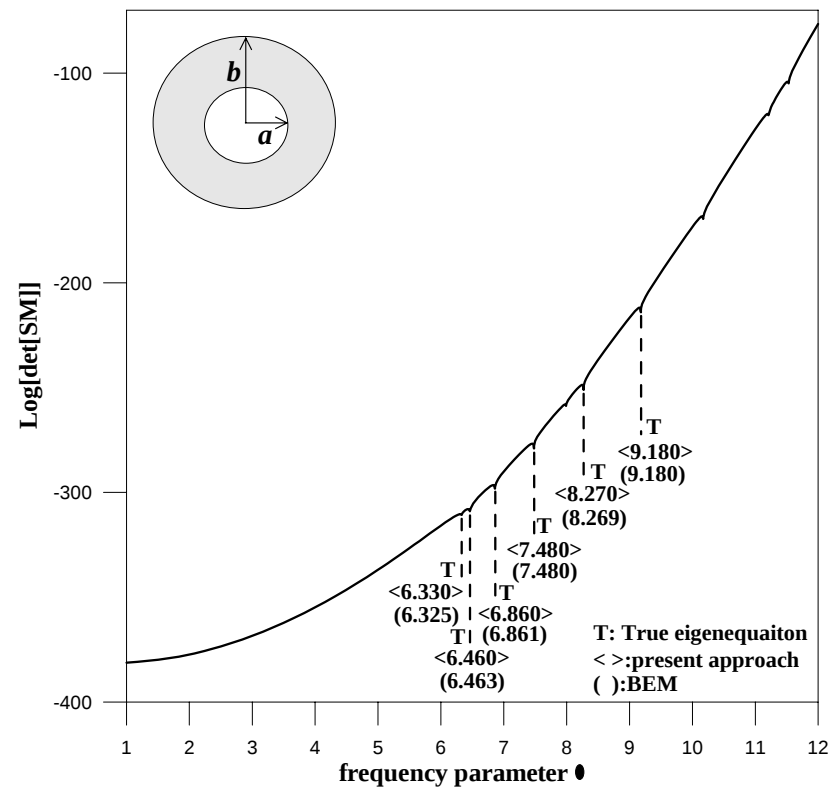




Multiply-connected plate



Clamped-clamped
boundary



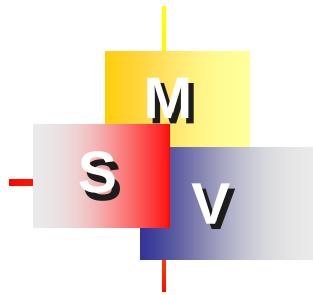
Simply-supported-simply-supported
boundary



ECCOMAS Thematic Conference on Meshless Methods 2005 ~ 44

Department of Harbor and River Engineering, Nation Taiwan Ocean University

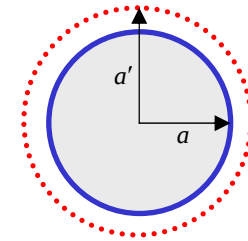




Method of solution

Membrane

For the Dirichlet problem ($u=0$) (Single-layer)



$$\{0\} = [U_{ij}]\{\phi_j\} \implies \det[U_{ij}] = 0$$

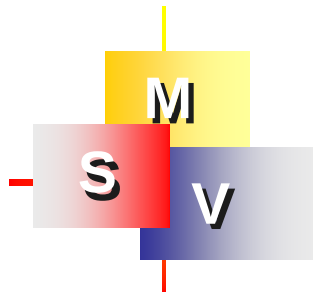
Plate

For the clamped boundary condition ($u=0, \theta=0$) ($U - \Theta$)

$$\begin{aligned} \{0\} &= [U]\{\phi\} + [\Theta]\{\psi\} \\ \{0\} &= [U_\theta]\{\phi\} + [\Theta_\theta]\{\psi\} \end{aligned} \implies \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} = \begin{bmatrix} U & \Theta \\ U_\theta & \Theta_\theta \end{bmatrix} \begin{Bmatrix} \phi \\ \psi \end{Bmatrix}$$

$$\det[SM_1^c] = 0$$





Degenerate kernels

Membrane

$$U(s, x) = \begin{cases} U^i(R, \theta; \rho, \phi) = \sum_{\ell=-\infty}^{\infty} J_{\ell}(k\rho)[iJ_{\ell}(kR) - Y_{\ell}(kR)]\cos(\ell(\theta - \phi)), & R > \rho, \\ U^e(R, \theta; \rho, \phi) = \sum_{\ell=-\infty}^{\infty} J_{\ell}(kR)[iJ_{\ell}(k\rho) - Y_{\ell}(k\rho)]\cos(\ell(\theta - \phi)), & R < \rho, \end{cases}$$

Plate

$$U^i(R, \theta; \rho, \phi) = \sum_{m=-\infty}^{\infty} \frac{1}{8\lambda^2} \{J_m(\lambda\rho)[Y_m(\lambda R) - iJ_m(\lambda R)] + \frac{2}{\pi}(-1)^m I_m(\lambda\rho)[(-1)^m K_m(\lambda R) - iI_m(\lambda R)]\} \cos(m(\theta - \phi)), \quad R > \rho,$$

$$U^e(R, \theta; \rho, \phi) = \sum_{m=-\infty}^{\infty} \frac{1}{8\lambda^2} \{J_m(\lambda R)[Y_m(\lambda\rho) - iJ_m(\lambda\rho)] + \frac{2}{\pi}(-1)^m I_m(\lambda R)[(-1)^m K_m(\lambda\rho) - iI_m(\lambda\rho)]\} \cos(m(\theta - \phi)), \quad R < \rho,$$

